"APPROVED FOR RELEASE: 08/09/2001

CIA-RDP86-00513R001860620015-2

VOLLEYDT 'inoral Nutrition

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Abs Jour : Rof Zhur - Biol., No 16, 25 Aug 57, No 68945

Author : Mosolov, I.V., Volloidt, L.F.

Title

: Entry of Sulfur Into Flants from Root and Abovo-Ground

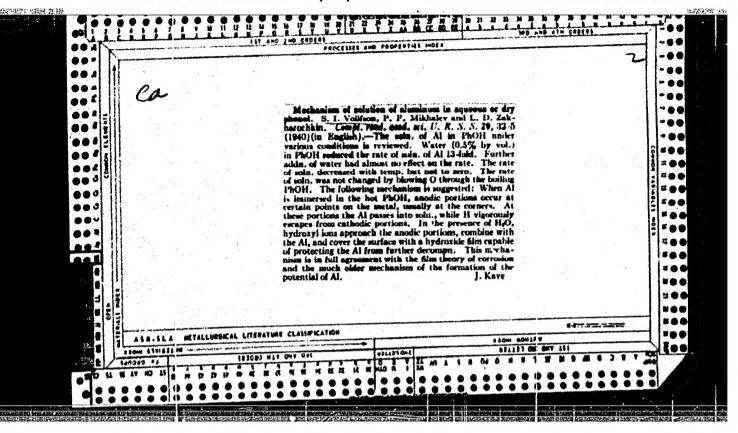
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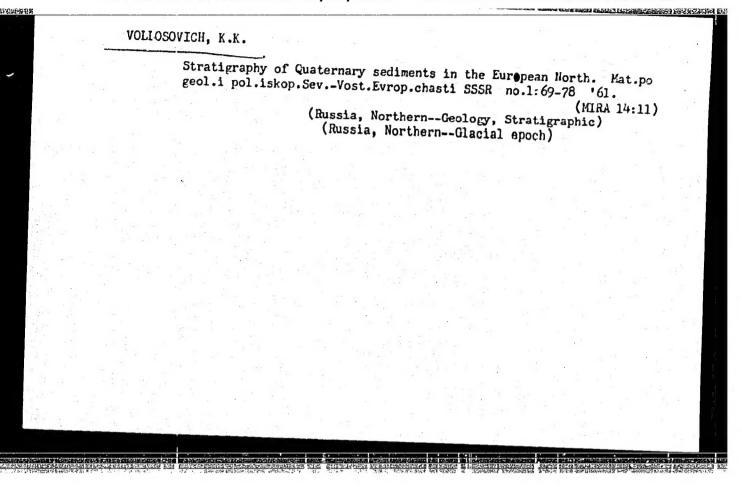
Orig Fub : Udobronie i urozhei, 1956, No 8, 13-17

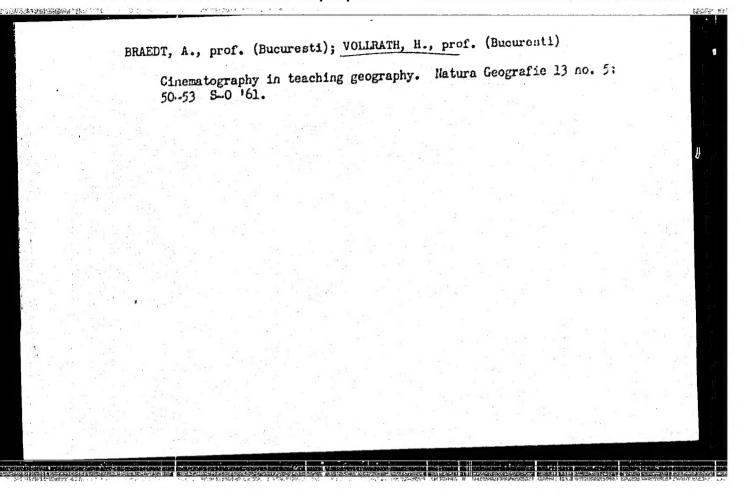
Abstract : In introducing solutions of K2S3504 on upper and lower loaves of beens it was found that after 12 days 335 from the upper young leef migretes in most cases into the beams, also into young leaves and rocts. From the old leaf S35 migrates into all parts of the plant, but to a lossor dogree into are parts of the plane, but to a lossor dogree into reproductive organs than the roots. In the experiment with introduction of K2S²O4 on a sunflower loaf it was found that S²D accumulated in the young growing loaf. In S²D root feeding of sunflower, it was shown that S²D accumulates mainly in young plent tissues, which ere distinguished by high intensity

of protein synthesis, end in the reproductive organs.

Card 1/1







VOLLSHKIM, [n.Ye., (st.Verkhniy Baskunchak); ANDRIYEVSKIY, V.G.; inshener
po remonth (st.Verkhniy Baskunchak)

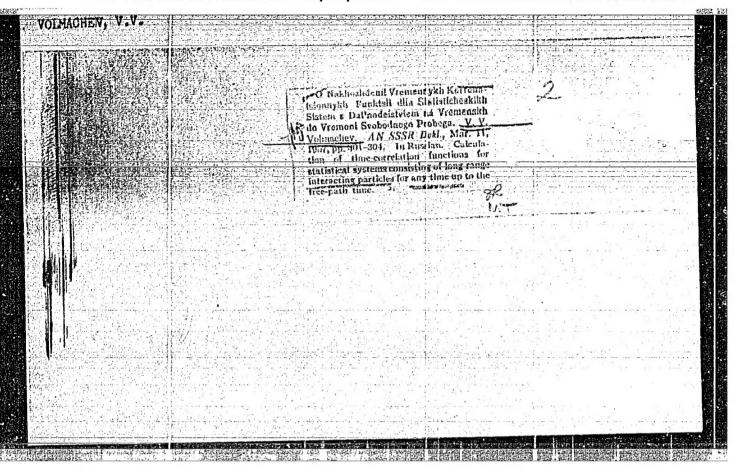
On the operation of ms generator diesel locomotives. Zhelador.
transp. 39 no.2:78 f '57.

1. Zamestitel' nachal'nika teplovomnogo depo.
(Diesel locomotives)

VOLLOSOVICH, K. A.

Geological Work on the Novosibirsk Islands. Izv. Akad. Nauk. Vol 16 No 5, 1902

SO: Trudy Arkitcheskogo Nauchno-Issledovatel'skogo Instituta, GUSMP, Council of Ministers, Vol 201, 1948

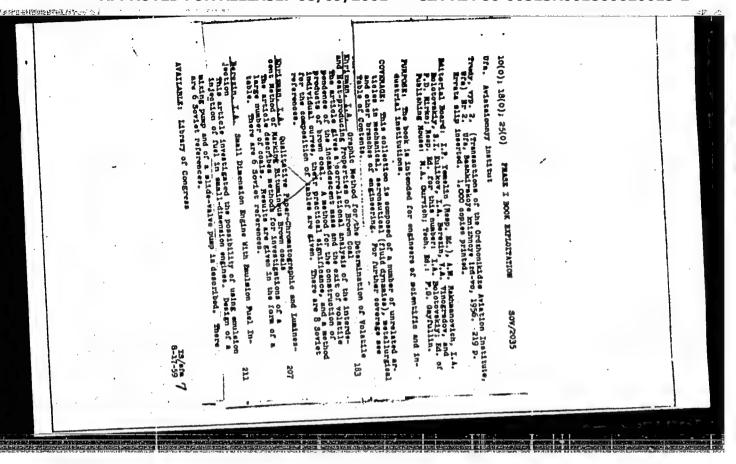


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S/124/61/000/008/013/042 A001/A101

AUTHOR:

Vol'man, B.L.

TITLE:

On one variation problem in dynamics of flight

PERIODICAL:

Referativnyy zhurnal. Mekhanika, no. 8, 1961, 28, abstract 8B169 ("Tr. Ufimsk. aviats. in-ta", 1957, no. 3, 211 - 221)

TEXT: The aim of this study is to determine optimum trajectories of aircraft vertical roll, the sequence of their calculations and the method of prescribing them to the pilot for their execution. In equations of aircraft motion, excessive thrust is held as a function of altitude and velocity of flight, the dependence of excessive thrust on normal overload is not taken into account. The determination of optimum trajectories is reduced to finding two functions of aircraft horizontal displacement, altitude and velocity of aircraft. These functions minimize time expenditure for horizontal displacements at the existence of non-holonomic connection, resulting from the motion equations, and at the given initial and final velocity values. The altitude attained during the aircraft evolution is a quantity sought for which is determined in the process of calculations. Euler's equations in this case are non-linear and are solved by numerical

Card 1/2

On one variation problem in dynamics of flight

S/124/61/000/008/013/042 A001/A101

methods. An example is given for a subsonic aircraft with a turbo-jet engine. The result of calculations and analysis of equations permit recommendation for execution of optimum vertical rolls at all altitudes with a constant normal overload equal to factor two.

G. Aronin

[Abstracter's note: Complete translation]

Card 2/2

SOV/123-59-16-63947

Translation from Referativnyy zhurnal, Mashinestroyeniye, 1959, Nr 16, p 45 (USSR)

AUTHOR:

Voltman, B.L.

TITLE

Inertia Accumulator With Hydraulic Drive

PERIODICAL

Sb. Ufimsk, gor. nauchno-tekhn. konferentaiya, posvyashch. vypolneniyu direktiv XX sayeda KPSS po tekhn. progressu v prom-sti, Ufa, 1957, 182-196

ABSTRACT:

A short investigation is made to determine the basic working rules of inertia accumulators with hydraulic drive. It is noted that the direct weights of devices for the storage of the same energy - in the form of elastically deformed steel, compressed air or high-speed rotating flywheel - are related to each other as 50:: 5:1. It is pointed out that the inertia accumulator (fly-wheel) permits in the simplest way to quickly the inertia accumulator (fly-wheel) permits in the simplest way to quickly store energy and to give back this stored energy with the aid of a hydromechanic transmission which is switched over automatically. The inmechanic transmission which is switched over automatically. The inconnected with a pump of complex hydrotransmission 2, which combines a connected with the shaft 4 of the transmission, which by way of G receives

Card 1/2

Inertia Accumulator With Hydraulic Drive

SOV/123-59-16-63947

the energy, stored by the flywheel. The flywheel itself is accelerated to maximum revolutions through the second T, the pump 5 of which is rigidly fastened to the shaft, but the turbine 6 of this T fits freely on the shaft and is rigidly fixed to the drive of the planetary multiplier 7. The introduction of the latter into the scheme is caused by the fact that the flywheel should generally be accelerated to maximum revolutions when the machine is working on the minimum number of revolutions, For the return of the stored energy of the flywheel, the transformer G is quickly filled up with oil, but T is emptied, 'In this way the flywheel transfers the stored energy to the transmission which is accelerated to a high number of revolutions. When the machine turns only slowly, G is free of oil and T works in a completely filled state with a minimum slide, and the flywheel is accelerated. In this way T is actually used for stepless regulation of the number of revolutions of the flywheel while the transmission is turning at variable speeds. In order to switch off the inertia accumulator, the oil is evacuated from T and G. The equation of motion of the system is derived, the expressions for determining the number of revolutions of the flywheel and transmissions and other parameters are given, which permit to compute the structural elements.

S.I.P.

Card 2/2

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SOV/124-58-8-8823

Translation from: Referativnyy zhurnal, Mekhanika, 1958, Nr 8, p70 (USSR)

AUTHOR:

Vol'man, B.L.

TITLE:

A Hydraulically Driven Inertial Accumulator (Inertsionnyy

akkumulyator s gidroprivodom)

PERIODICAL:

V sb.: Ufimsk. gor. nauchno-tekhn. konferentsiya, posvyashch. vypolneniyu direktiv XX s"yezda KPSS po tekhn.

progressu v prom-sti. Ufa, 1957, pp 182-196

ABSTRACT:

In the operation of many machines the necessity exists for storing up energy so that at a given time it can be quickly released for the purpose of accelerating the machine's action. Energy of this type, i.e., for storage, can be accumulated mechanically either in the form of the potential energy of an clastically deformed body or in that of the kinetic energy of a rapidly turning flywheel. Both of these methods involve increasing the weight of the machine. If the three energystorage devices --- functioning on the principle of elastically deformed steel, compressed air, and a rapidly turning flywheel, respectively --- were to store the same amount of energy,

Card 1/2

SOV/124-58-8-8823

A Hydraulically Driven Inertial Accumulator

the ratio of their direct weights would be 50:5:1, respectively. Hence, the most efficient method for storing up energy is with an inertial accumulator, which makes it possible by simple means, with the aid of automatic-shift fluid couplings, to store and release energy quickly. The author investigates the performance of an inertial energy accumulator of this type having a hydraulic drive system consisting of a hydraulic torque converter. Investigated also are the laws that govern the operation of an inertial energy accumulator, and the author works out the design relationships needed for the creation of such a device. It is stressed that, when for a hydraulically driven inertial accumulator the optimal parameters are selected, 60-70% of the stored-up energy is transmitted to the machine, with 25-30% passing off as heat and approximately 7-10% remaining unused.

Yu.A. Lashkov

Card 2/2

AZBUKIN, Yu.I. inzhener; VOL'MAN, O.L., inzhener.

Self-uncoupling coupling of electric starting motors for synchronous compensators. Elek.sta. 26 no.6:52-53 Je '55.

(Electric motors)

(Electric transformers)

(Electric transformers)

ORLOVA, L.M., inzh.; YEVSTRATOVA, V.M., inzh.; VOL'HAN, I.A., tekhnik

Electrolytic polishing of certain die steels. [Nauch. trudy]

ENIKMASha 7:135-139 '63. (MIRA 16:7)

(Tool steel) (Electrolytic polishing)

AVERTYANOVA, L.L.; FIDELTMAN, Ye.S.; VOLTMAN, T.B.

Changes in the content of lysozyme in the saliva of rheumatic children under the effect of bicillin therapy. Antibiotivi 10 no.5:445-447 My *65. (M.RA 18:6)

1. Laboratoriya immunopatologii sardechno-sosudistoy sistemy (zav. - prof. D.F.Pletsityy) Instituta normalinoy i patologicheskoy fiziologii AMN SSSR i Detskaya poliklinika No.30, Moskva.

TUROVA, F.D.; EOTUNOVA, L.M.; BOSIK, R.N.; DEMCHENKO, M.P.; VOL'MAN, I.B.

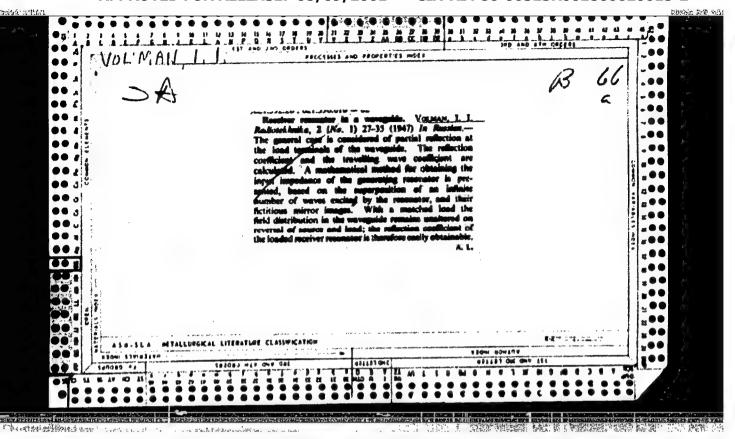
Care of convalescents following pneumonia. Pediatrila 38 no. 3:72-75
Mr '60. (PNEUMONIA)

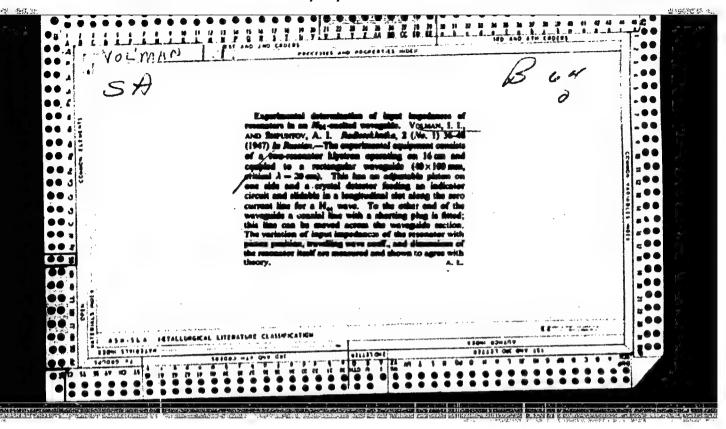
(PNEUMONIA)

VOL'MAN, I.I.

Trends in knitwear styles for 1966. Tekst. prom. 25 no.9: 26-29 S 165. (MIRA 18:10)

1. Olavnyy khudoshnik Doma modeley trikotashnoy promyshlennosti.





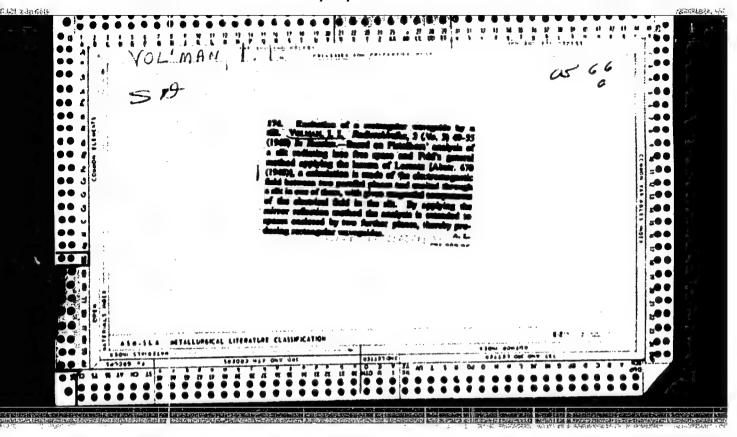
VOL'MAN, I.T.

Styles in knit wear for 1962. Tekst.prom.22 no.3:15-18 Mr '62.

(MIRA 15:3)

1. Khudozhestvennyy rukovoditel' Doma modeley trikotazhnykh izdeliy.

(Fashion)(Knit goods)



VOL'MAN, I.I.

Krit goods styles in 1963. Tekst.prom. 23 no.5:39-43 My '63.

(MIRA 16:5)

1. Glavnyy khudozhestvennyy rukovoditel' Vsesoyuznogo Doma modeley trikotazhnykh izdeliy.

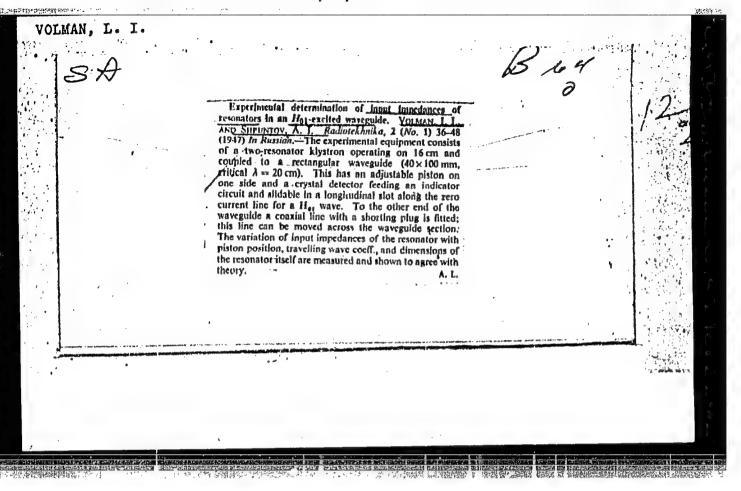
(Knit goods) (Fashion)

Outbreak of streptococcal food infection. Gig. 1 san. 24 no.5:58-59
Hy '59.

1. Iz Moskovskoy gorodskoy sanitarno-enidemiologicheskoy stantsii.

(STHENTOCOGGAL INFECTIONS, epidemiology,
food pois. outbreak (Rus))

(POOD POISONING, epidemiol,
streptococcal outbreak (Rus))



GUREVICH, Lev Isayevich, kand. tekhn. nauk; MATKHANOV, Vasiliy Nikolayevich, inzh.; SAVIN, M.G., inzh., retsenzent; VOL'MAN, L.N., red.

[Masters of the blue flame] Mastera golubogo ognia. Irkutsk, Vostochno-Sibirskoe knizhnoe izd-vo, 1964. 77 p. (MIRA 18:3)

KRASROV, Izrail' Davidovich, kand. ekon. nauk; VOLIMAH, I.N.,

Methods of raising the scientific level of capital construction planning; based on materials of the East Ciberian Economic Region] Puti povyshenila nauchnogo provnia planirovanila kapital nego stroitel stva; po materialam Vostochno-Sibirskogo ekonomicheskogo raiona. Irkutsk, Vostochno-Sibirskoe knizhnoe izd-vo, 1964. 149 p. (MIRA 18:6)

VOLIMAN, L.O.

Result of antituberculosis vacination in rural area [with summary (HIRA 11:10) in French]. Probletuh. 36 no.6:13-15 58

1. Glavnyy vrach rayona Kremennoye Luganskoy oblasti, USER. (BCG VACCINATION. in Russia (Rus))

Effect of the nonsymmetry of magnetomotive forces on the equalizing currents in d.c. machinery with ordinary armature winding. Trudy LTITSBP no.10:105-117 '62. (MIRA 16:8)

(Electric motors, Direct current)

VOL'MAN, Nikolay Stanislavovirn; GRACHEV, A.I., red.

[Electric power supply of woodpulp and paper enterprises]
Elektrosnabzhania taolliulozno-bumazhrykh predpriiatii.

Moskva, Lesnaia promyshlennost', 1962. 349 p.

(MIRA 17:11)

BUSHMELEV, Vasiliy Afenas'yevich; VOL'MAN, Nikolay Stanislavovich;
BALLIASOV, Ye.Ya., red.; FEDOROV, B.M., red.izd-ve; KOHNYUSHIHA,
A.S., tekhn.red.

[Processes, equipment, and machinery of the woodpulp and paper industry; textbook for special secondary schools] Protsessy, apparaty i oborudovanie tselliulozno-bumazhnogo proizvodstva; uchebnik dlia srednikh spetsial nykh uchebnykh zavedenii.

Moshva. Goslasbumisdat, 1960. 422 p. (MIRA 13:11)

(Paper industry--Equipment and supplies)

KULIKOVSKIY, Petr Konstantinovich, kand. tekhn.nauk; SHUSTOV,
Aleksandr Dmitriyevich, inzh.; VOL'MAN, N.S., red.;
SOBOLEVA, Ye.M., tekhn. red.

[Electric drives for machinery in the cellulose and paper-making industry] Elektroprivod mashin tselliulozno-bumazhnoi promyshlennosti. Moskva, Gosenergoizdat, 1962.
371 p. (MIRA 16:4)

(Cellulose) (Paper-making machinery--Electric driving)

VOL'MAN, S.B.

Small 2 ton-capacity fork lift truck. Avt. prom. 30 nc.7:47 Jl 164. (MIRA 17:9) 1. Glavnoye spetsial noye konstruktorskoye byuro po avtopogruzchikam.

KIRPICHNIKCV, O.B.; VOL'MAN, V.G.

Use of a VICKhOM penetratometer for determining soil density up to 60 cm. Trakt. i sel'khozmash. 31 no.12:18 D '61. (HIRA 15:1)

1. Spetsial'noye konstruktorskoye byuro zavoda im. Oktyabr'skoy revolyutsii. (Soil mechanics)

"APPROVED FOR RELEASE: 08/09/2001

CIA-RDP86-00513R001860620015-2

13+1

L 05731.67 EAT(1) GD

ACC NR. AT6022276

SOURCE CODE: UR/0000/66/000/000/0057/0062

AUTHOR: Voltman, V. I.; Muravtsov, A. D.

ORG: none

TITLE: Calculation of the ferrite-and-dielectric-loaded waveguide Y-circulator

SOURCE: Vsesoyuznaya nauchnaya sessiya, posvyashchennaya Dnyu radio. 22d, 1966. Sektsiya kvantovoy elektroniki. Doklady. Moscow, 1966, 57-62

TOPIC TAGS: waguide circulator, waveguide element

ABSTRACT: Circulation equations for a Y-circulator with a ferrite cylinder inside a dielectric bushing are set up; assumptions: (a) the amplitude of the first azimuth harmonic of the electric field on the bushing surface substantially exceeds the amplitudes of all other harmonics; (b) one of the nodes of the standing wave formed on the bushing surface is located along the axis of the arm being isolated. The equations contain 7 independent parameters; 5 of them must be specified, and 2 can be found from the solution. The parameter selection is limited by the requirement that the isolation between the circulator arms should be 20 db or more. A calculation procedure and auxiliary curves are supplied. An experimental verification is claimed which revealed errors of 8—20% between theoretical and experimental values.

Orig. art. has: 4 figures and 5 formulas.

SUB CODE: 09 / SUBM DATE: 11Apr66 / ORIG REF: 001 / ATD PRESS: 5046

Card 1/1 pla

VOL'MAN, V.I.

Ferrite switches. Radiotekhnika 18 no.8:24-30 Ag '63.

(MIRA 16:10)

1. Deystvitel'nyy chlen Nauchno-tekhnicheskogo obshchestva radiotekhniki i elektrosvyazi imeni Popova.

BR

ACCESSION NR: AP4026145

5/0108/64/019/003/0019/0024

AUTHOR: Vol'man, V. I. (Active member)

TITLE: Principle of operation and design method of waveguide Y-circulators

SOURCE: Radiotekhnika, v. 19, no. 3, 1964, 19-24

TOPIC TAGS: waveguide, waveguide circulator, waveguide Y circulator, waveguide junction, ferrite in waveguide

ABSTRACT: The functioning of an H-plane Y-junction circulator with a ferrite placed at its center is explained. The circulator can be used as a high-speed microwave switch without any moving mechanical parts. It is assumed that the electric-field-intensity distribution at the dolted line (see Enclosure 1) is proportional to this function:

$$f_1(x) = \begin{cases} \sin \frac{2\pi x}{a_1} & \text{with } 0 < x < \frac{a_1}{2} \\ 0 & \text{with } \frac{a_1}{2} < x < a_1 \end{cases}$$

Card 1/3

ACCESSION NR: AP4026145

when the energy is admitted to the arm 2. Frequency variation brings about a change in the phase velocity and the coupling factor of H_{20} , H_{30} , and H_{10} modes. The best ferrite shape must result in a minimum change of the above parameters. The method of cross sections (K. A. Barsukov, Radiotekhnika i elektronika, v. 4, no. 8, 1959) is used for analyzing the operation and calculating the circulators. The method is valid for any shape of the ferrite element. Orig. art. has: 7 figures and 13 formulas.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi (Scientific and Technical Society of Radio Engineering and Electrocommunication)

SUBMITTED: 21Dec62

DATE ACQ: 16Apr64

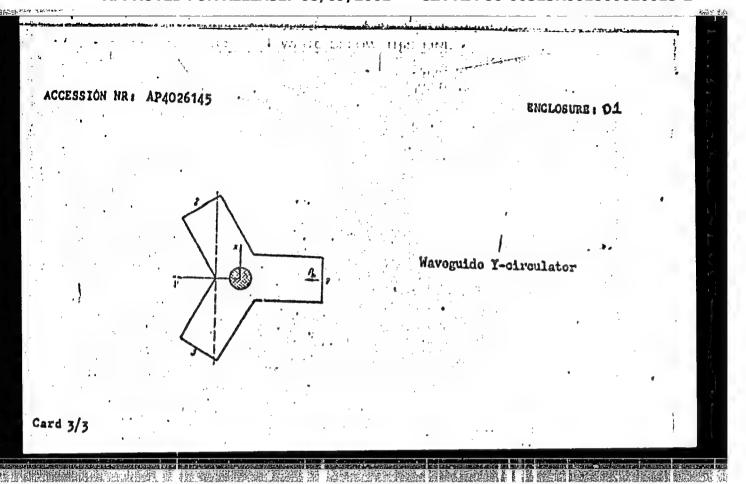
ENCL: 01

SUB CODE: ED

NO REF SOV: 004

OTHER: 003

Card 2/3



L 41550-65 ENT(1)/SEC-4/ENA(h) P=-4/Fac-4/Peb/Pi-4/P3-4 ACCESSION NR: JP5009074 UR/0108/65/020/003/0021/0030

31

AUTHOR: Vol'mail. V I (Active member)

TITLE: Design of a waveguide Y-circulator

SOURCE: Radiotekhnika, v. 20, no. 3, 1965, 21-30

TOPIC TAGS: Y circulator, waveguide circulator

ABSTRACT: A number of Western and Soviet articles have suggested formulas for designing Y-circulators which yield inadequate results. The present article offers an approximate method of design based on the presumption that the structure of the electric field at the ferrite-cylinder surface is similar to the structure resulting from the diffraction of a plane wave by a magnetized ferrite cylinder. This ing from the diffraction of a plane wave by a magnetized ferrite cylinder. This field distribution was verified experimentally on a slightly modified J. H. Collins, field distribution was verified experimentally on a slightly modified J. H. Collins, field distribution are et al. hookup (Electronic Engg., v. 35, no. 426, 1963). These conclusions are offered: (1) With definite relations between the ferrite parameters and dimensions, an electric-field standing wave is established at the ferrita-cylinder surface; an electric-field standing wave is established at the ferrita-cylinder surface; an electric-field standing wave is established at the ferrita-cylinder field distribution (2) Application of an external magnetic field turns the electric-field distribution curve about the cylinder axis through an angle θ_0 proportional to the magnetic-

Card 1/2

L 41550-65 ACCESSION HR: AP5009074

field strength; (3) Necessary and sufficient conditions for normal operation of a Y-circulator are given by formulas 14 and 15; (4) The band width of a Y-circulator depends on the ferrite dielectric constant: with lower constants the band is wider; (5) The power loss in a Y-circulator is largely determined by the magnetic loss in the ferrite and by its dielectric constant. "In conclusion, the author wishes to thank G. Z. Ayzenberg and V. V. Kikol'skiy for their valuable hints during a discussion and to R. I. Perets for his great help and constant attention. Orig. art. has: 11 figures and 30 formulas.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi im. A. S. Popova (Scientific and Technical Society of Radio Engineering and Electrocommunication)

SUBMITTED: 15Dec63

ENCL: 00

SUB CODE: EC

NO REF SOVI 005

OTHER: 006

ATD PRESS: 325

"APPROVED FOR RELEASE: 08/09/2001

CIA-RDP86-00513R001860620015-2

L 28516-66 EWA(h)/EWT(1) SOURCE CODE: UR/0108/66/021/002/0031/0035 ACC NR: AP6007151 AUTHOR: Vol'man, V. I. (Active member) ORG: Scientific and Technical Society of Radio Engineering and Electrocommunication (Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi) TITLE: Waveguide Y-circulator with a sphere SOURCE: Radiotekhnika, v. 21, no. 2, 1966, 31-35 waveguide circulator, ferrite circulator, waveguide TOPIC TAGS: waveguide. element, electromagnetic wave diffraction, standing wave ABSTRACT: The ferrite-sphere diameter is found by solving a problem of diffraction of electromagnetic waves by a dielectric sphere and by formulating the conditions of existence of a standing wave of the first field harmonic on the sphere surface. The wave arriving at the sphere is assumed to be planar, and the effect of the waveguide metal walls on both sides of the sphere is neglected (the Card 1/2 UDC: 621.372

L 28516-66

ACC NR: AP6007151

introduced error is 10-15%). The condition of an electric standing wave on the sphere surface (with a TE₁₀-mode in one of the circulator arms) is described by a differential equation; the roots of this equation given as curves permit determining the sphere diameter. An experimental verification with a ferrite sphere of 8.95-rm diameter at 10.557 Gc is reported. The circulator frequency band was widened (to 11.5%) by slipping a polystyrene bushing over the ferrite sphere. No appreciable parameter variation was observed within +15+70C temperature change or ±10% magnetic field variation. "The author wishes to thank A. D. Muraytsev for his great help in experimental work." Orig. art. has: 7 figures and 8 formulas.

SUB CODE: 09 / SUBM DATE: 05Jun64 / ORIG REF: 003

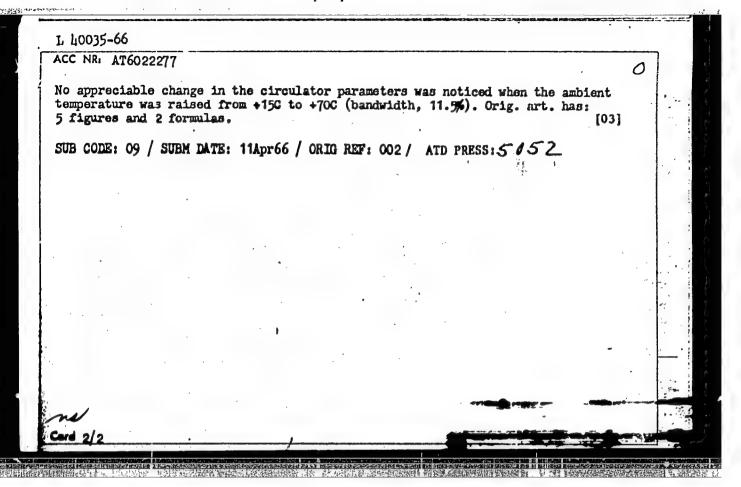
Card 2/2 CC

L 40035-66 EWT(1) SOURCE CODE: UR/0000/66/000/000/0063/0069 ACC NR: AT6022277 AUTHOR: Vol'man, V. I. ORG: none TITLE: Waveguide Y-circulator with a sphere SOURCE: Vsosoyuznaya nauchnaya sessiya, posvyashchonnaya Dnyu radio. 22d. 1966. Sektsiya kvantovoy elektroniki. Doklady. Moscow, 1966, 63-69 TOPIC TAGS: waveguide circulator, waveguide element , FERRITE ABSTRACT: It is assumed that the physical processes transpiring in a Y-circulator containing a ferrite sphere are qualitatively equal to those in the circulator containing a ferrite cylinder. In calculating the ferrite sphere size, the equations valid for a dielectric sphere are used, and the conditions of formation of the standing wave of the first electric-field harmonic, on the sphere surface in the planes parallel to equatorial, are assumed. The ferrite-sphere circulator may prove particularly suitable for the millimeter-band equipment because of easier manufacture of small forrite spheres than cylinders. In an experimental varification, a M-188, 8.95-mm diameter, E = 11.6 sphere in a 650-ce field ensured a maximum isolation of

35-40 db at 10557 Mc; the passband was fairly narrow. A second isolation maximum

at 10757 Mc, 1000-eo was observed. An experimental plot of electric-field distribution at the ferrite-sphere surface in the tuned circulator is shown.

Card/2



"APPROVED FOR RELEASE: 08/09/2001

CIA-RDP86-00513R001860620015-2

IJP(c) EWT(1) L 46194-66 UR/0108/66/021/007/0067/0068 ACC NR: AP6023861 SOUR 54 AUTHOR: Vol'man V. I. (Active member) and Electro-Communications ORG: Scientific and Technical Society radiotekhniki i elektrosvyazi) im. A. S. Fopov (Nauchno-tekhnicheskiy TITLE: Procedures for the control of the paneters of ferrite cylinders SOURCE: Radiotekhnika, v. 21, no. 7, 1966, 67-68 TOPIC TAGS: ferrite, waveguide, waveguide frequency, frequency control, resonator ABSTRACT: The parameters of each ferrite cylinder to be used in a waveguide Y-circulator must be controlled very accurately if good reproducibility of the circulators is to be insured. The author outlines a method for controlling the parameters of the ferrite cylinders to the point that Y-circulators can be reproduced with an optimal tuning frequency deviation of less than *0.5%. The method makes use of a resonator which is so designed and constructed that any deviation in the parameters of the ferrite cylinder influences the frequency of oscillation of the resonator by an amount equal to the influence the same deviation would have on the optimal tuning frequency of the Y-circulator. Formulas for the optimal tuning frequency and the oscillation frequency of the resonator are shown to have the same dependence upon the parameters of the ferrite cylinder. The relationships were examined experimentally and found to agree very closely with those predicted. The effects of the ellipticity of the fer-UDC: 621.396.677 Card 1/2

quency of author of versely	of the circ concludes t affects th	ulator are di hat it is dif	scussed. On ficult to sh lity of the	der in the ci the basis of ow which of t tuning freque	experiment the ferrite	al results, parameters	the most ad-
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CIA-RDP86-00513R001860620015-2

I, 09970-67 EET(1) GD ACC NR. AT6022279 SOURCE CODE: UR/0000/66/000/00079/0082

AUTHOR: Vol'man, V. I.; Muravtsov, A. D.

ORG: none

TITLE: Methods of parameter control in ferrite cylinders used in waveguide Y-circu-

lators

SOURCE: Vsesoyuznaya nauchnaya sessiya, posvyashchennaya Dnyu radio. 22d. 1966.

Sektsiya kvantovoy elektroniki. Doklady. Moscow, 1966, 79-82

TOPIC TAGS: waveguide, waveguide propagation, waveguide design, ferrite

ABSTRACT: A method for testing ferrite cylinders prior to their installation in circulators is reported. The method consists of placing ferrite cylinders into a specially designed resonant cavity and measuring the resonant frequency of this system. This approach helps to increase ferrite component yield in mass production. Rather than measure the absolute values of resonance, the deviation from a standard reference value is determined. For a cylindrical resonant cavity with a coaxial internal magnetized ferrite cylinder, electromagnetic waves can be sustained if the following relation is satisfied:

 $\frac{I_{n}(x_{0}/\ell)}{Y_{n}(x_{0}/\ell)} = -\frac{I_{n}(x_{0}r_{1})}{Y_{n}(x_{0}r_{1})} - \frac{2}{\pi x_{0}r_{1}Y_{n}^{2}(x_{0}r_{1})} \times \frac{1}{\frac{\eta_{0}}{\eta_{1}} \left[\frac{I_{n}'(r_{\perp}r_{1})}{I_{n}(x_{\perp}r_{1})} - \frac{k}{\mu} \frac{n}{x_{\perp}r_{1}}\right] - \frac{Y_{n}(x_{0}r_{1})}{Y_{n}(x_{0}r_{1})}}$ (1)

Card 1/2

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ACC NR: AT6022273

where R is the radius of the cavity, r_1 is the radius of the ferrite cylinder. If the resonator dimensions are selected such that $Y_1(x_0R) = 0$, (2)

then, according to (1) for $n = \pm 1$ at resonant frequency the expression (3) must be true.

 $\frac{\eta_0}{\eta_1} \left[\frac{I_1'(x_1r_1)}{I_1(x_1r_1)} \pm \frac{k}{\mu} \frac{1}{x_1r_1} \right] = \frac{Y_I'(x_0r_1)}{Y_1(x_0r_1)}, \quad (3)$

The numerical computation shows that for $|k/\mu| = 0.5$ to 0.6 the half sum of the resonant frequencies approximately coincides with the roots of the equation

$$\frac{\eta_0}{\eta_\perp} \frac{I_1'(x_\perp r_1)}{I_1(x_\perp r_1)} = \frac{Y_1'(x_0 r_1)}{Y_1(x_0 r_1)}. \tag{4}$$

It is known that this expression is nearly the same as the one for the operation of a Y-circulator equipped with a ferrite cylinder having optimum properties. Consequently, the ferrite cylinders can be selected for optimum performance on the basis of the indirect measurement of their electrical parameters, using the resonance method. The experimental evaluation of 40 ferrites has shown this test to be highly accurate and useful. Orig. art. has: 5 figures.

SUB CODE: 09,17/

SUBM DATE: 11Apr66/

ORIG REF: 001

Card 2/2 5/10

SKIYAROVA, V.K., otv. red.; ARALOVA, V.I., red.; VOL'MAN, V.K., red.;
DERZHAVIN, B.A., red.; IVANOVA, V.A., red.; KOMAROVA, V.R.,
red.; KULICHEV, A.F., red.; MAKAROVA, H.S., red.; NARODETSKIY,
red.; PROKOF'YEVA, T.I., red.; PROZOROVA, T.A., red.;
RAZUMOVSKAYA, S.V., red.; RODIONOV, V.A., red.; SURGUNOVA,
N.S., red.; KHVOSTOV, V.V., red.; KLEYMENOVA, T.A., tekhn. red.

[Men's clothing] Muzhskaia odezhda. Moskva, 1961. 27 p. (MIRA 15:2)

1. Russia (1923- U.S.S.R.) Gosudarstvennaya planovaya kommissiya. Vsesoyuznyy institut assortimenta izdeliy legkoy promyshlennosti i kul'tury odezhdy. (Men's clothing)

VOLUME, Z. G. O primonenia polvodnov kishachnov vanny. Trudy dlav. voyen. Gespitalye Veoruck. Sil. SSS2 in. akad. Burdenko. V.F. 6 kt., 12/9, S. 258-65.

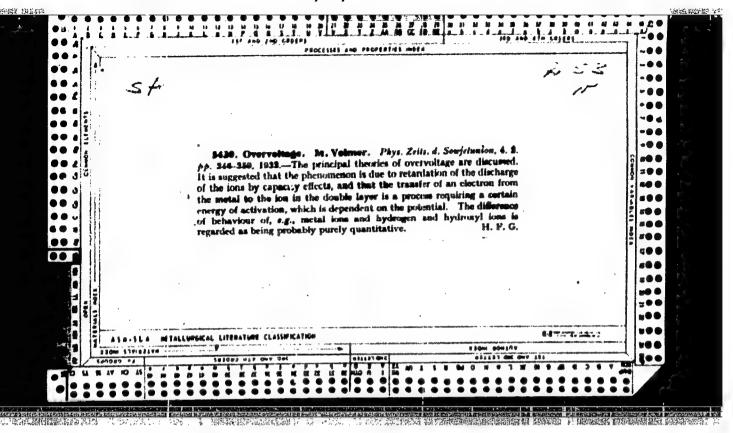
SC: Letopis, No. 32, 19/9.

VOL'MAI, Z. Ya.

24341

VOL'MAN, Z. Ya. Opyt primeneniya torfa-syrtsa v usloviyakh armeyskogo gospitalya legko ranenysh. Trudy Glav. voyen. Gospitalya Vooruzh. Gil. SSSL im. akad. Eurlenko. VIP. 6. H., 1949, 3. 159-62.

50: Letopis, No. 32, 1949.



VOLMER, Y.

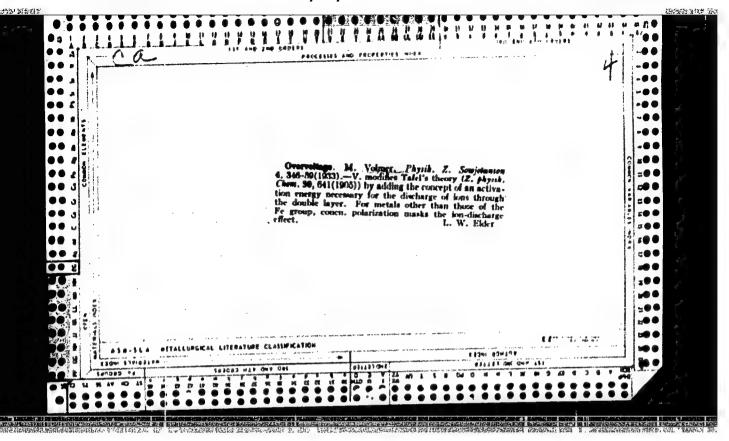
J. Volmer, "A Simple Geometric Method for the Synthesis of Planar Mechanisms."

paper presented at the 2nd All-Union Conf. on Fundamental Problems in the Theory of Machines and Machanisms, Moscow, USSE, 24-28 March 1958.

BURSIAN, N.R.; MASLYANSKIY, G.N.; Prinimal uchastiye: VOLMIKHINA, N.K.

Gatalytic isomerization of n-pentane on a platinum catalyst. Khim.
prom. no.3:166-168 Mr '61.
(Pentane)

(Pentane)



VOL'MIR, A. S.

Privedennaia shirina ploskoi paneli pri odnovremennom deistvii szhatiia i sdviga. (Moscow. Voennaia vozdushnaia akademiia Krasnoi Armii. Nauchnotekhnickeskaia konferentsiia, 19hh g. Trudy, 19h5, v.2 Samoletnaia sektsiia, no. 2, p. 85-95, diagrs.)

Title tr.: Reduction coefficient of a flat panel subject to simultaneous compression and shear.

UG630.M67 v. 2, no. 2

SO: Aeronautical Sciences and Aviation in the Soviet Union, Library of Congress, 1955.

VOL'MIR, A. S.

O na priazhenijakh v szhatoj tsilindricheskoj paneli posie poteri ustojchivosti. (Moscow. Voennaja vozdushnaja akademija Krasnoj Armij. Nauchno-tekhnicheskaja konferentsija, 1944 g. Trudy, 1945, v.2: Samoletnaja sektsija, no. 2, p. 145-157, diagrs.)

Title tr.: Tension in a compressed cylindrical panel after buckling.

UG630.M67 v.2, no.2

SO: Aeronautical Sciences and Aviation in the Soviet Union, Library of Congress, 1955.

FA 16/49 55

USSR/Engineering Plasticity

Jul 48

"Important Contribution to Soviet Science,"
Docent A. Volmir, Cand Tech Sci, It Col Engr Ye.
Kononenko, Docent, Cand Tech Sci, 52 pp

"Vest Vozdush Flota" No 7 (352)

Summarizes A. A. Il'yushin's work on theory of plasticity. Although a complete translation of Il'yushin's paper was published in US in 1947 (NACA Technical Note No 1115), certain American authors do not acknowledge their indebtedness to him.

FIB

16/49755

KORDNEY, E.G., doktor tekhnicheskikh mauk, professor, redaktor; VOLIMIR, A.S., kandidat tekhnicheskikh mauk, redaktor.; PULIMIR, Tel.A., tekhnicheskiy redaktor.

11 -9 111 21

[Studies in the dynamics of structures] Issledovaniia podinamike soorushenii. Pod red. B. G. Koreneva. Moskva, Gos. izd-vo stroitel noi lit-ry. 1951. 159 p. (MLRA 8:9)
[Microfilm]

NOLYAJR.

BABKIN, S. I., kandidet tekhnicheskikh nauk; BalakeHIN, B.S., professor, doktor tekhnicheskikh nauk; BEYZEL MAN, R.D., inzhener; BELYAYEV. Y. W., kendidat tekhnicheskikh neuk; BIRGEP, I.A., kendidat tekhnicheskikh nauk; BCGUSIAVSKIY, P.Ye., kandidat tekhniceskikh nauk; BOROVICH, L.S., kandidat tekhnicheskikh nauk; VOL'KIR, A.S. professor, doktor tekhnicheskikh nauk; GONIKHERG, Yu.H., inzhener; GORODETSKIY, I.Ye., professor, doktor tekhnicheskikh nauk; GORDON, V.O., professor; DIMENTRERG, F.H., kandidat tekhnicheskikh nauk; DOSCHATOV, V.V., inzhener, IVANOV, A.G., kandidat tekhnicheskikh nauk; KIMASOSHVIII. R.S., professor; KODNIR, D.S., kondidet tekhnicheskikh nauk; KOLOMIYTSEV. A.A., kandidat tekhnicheskikh nauk; KRUTIKOV, I.P., kandidat tekhnicheskikh nauk; KUSHUL', M.Ya., kandidat tekhnicheskikh nsuk; LEVENSON, Ye.M., inzhener; MAZYRIE, I.V., inshener; Mallbill, N.B., kandidat tekhnicheskikh nauk; MARTYBOV, A.D., kandidat tekhnichenkikh nauk; MIBERG, H.Ya., kandidat tekhnicheskikh nauk: NIKOIAYEV, G.A., professor, doktor tekhnicheskikh nauk; PRIRUSEVICH, A.I., doktor tekhnicheskikh nauk; POZDHYARGV, S.H., dotsent: PONAMOREV, S.D., professor, doktor tekhnicheskikh neuk; PRIGOROVSKIY, M. I., professor, doktor tekhnicheskikh nauk; PROKIN, B.A., kandidat tekhnicheskikh nauk; RESHETOV, D.N., professor, doktor tekhnicheskikh nauk; SATEL', E.A., professor, doktor tekhnicheskikh nouk; SERBESEN, S.V.; SLOBODKIN, M.S., inzhener; SPITSYN, N.A., professor, doktor tekhnicheskikh nauk; STOLBIN, G.B., kandida t tekhnicheskikh nauk; TAYTS, B.A., kandiat tekhnicheskikh nauk; TETEL'BAUN, I.M., kendidet tekhnicheskikh nauk; UMARSKIY, A.A., professor, doktor tekhnicheskikh nauk; FEODOS TEV, V.I., professor, doktor tekhnicheskikh nauk; (Continued on next card)

BABKIN, S.I.-- (continued) Card 2.

EMATT, D.M., kandidat teknicheskikh nauk; EMBIROV, V.N., kandidat teknicheskikh nauk; SHENDROV, V.S., kandidat teknicheskikh nauk; SHENDROV, V.S., kandidat teknicheskikh nauk, nauchwy redaktor; TSVETKOV, A.P., deteant, mauchwy redaktor; SLELNIKOV, J.I., inzhener, nauchwy redaktor; SLELNIKOV, J.I., inzhener, nauchwy redaktor; SUKEROL, H.S., doktor skiy redaktor

[Hanual of machirary manufacture] Spreatchik machinastreitelia; v trekt tomski, Moskva, Gos.manchno-teknicid-vo taskinastreitelia; lib-ry, Vol.3, 1951 1999 9.

[Hanual of machirary manufacture] Spreatchik machinastreitelia; lib-ry, Vol.3, 1951 1999 (MD. 1099)

[Handiday)

UMANSKIY, A.A.; AFANAS'YEV, A.M.; VOL'MIR, A.S.; GRIGOR'YEV, Yu.P.; KODANEV, A.I.; MAR'IN, V.A.; PRIGOROVSKIY, N.I.; SNITKO, I.K., redaktor; AKHLAMOV, S.N., tekhnicheskiy redaktor.

[Collection of problems on the strength of materials] Sbornik zedach po soprotivleniiu materialov. Moskva, Gos. izd-vo tekhn.-teoret. lit-ry, 1954. 480 p. (MLRA 7:12)

THE PROPERTY OF THE PROPERTY O

ANDREYEV, L.Ye., kandidat tekhnicheskikh nauk; BIDEMAN, V.L., kandidat tekhnicheskikh nauk; BOTARSHIMOV, S.V., kandidat tekhnicheskikh nauk; VOL'MIR, A.S., doktor tekhnicheskikh nauk; DIMENBERG, F.M. kandidat tekhnicheskikh nauk; ZASELATELEV, S.M., inshener; EINASOSHVILI, R.S., doktor tekhnicheskikh nauk, professor; EOVALENKO, A.D., MAKUSHIN, V.M., kandidat tekhnicheskikh nauk MALININ, N.N., kandidat tekhnicheskikh nauk; PONOMAREV, S.D., doktor tekhnicheskikh nauk; PRIGOROVSKIY, N.I., doktor tekhnicheskikh nauk; TETEL'BAUM, I.M., kandidat tekhnicheskikh nauk; UMANSKIY, A.A., doktor tekhnicheskikh nauk, professor; FEODOS'YEV, V.I., doktor tekhnicheskikh nauk; SERENSEN, S.V., redaktor; TRAPEZIN, I.I., kandidat tekhnicheskikh nauk, redaktor; KARGANOV, V.G., inshener, redaktor; SOKOLOVA, T.F., tekhnicheskiy redaktor.

[Mechanical engineer's manual; in 6 volumes] Spravochnik mashinostroitelia; v shesti tomakh. Ixd.2-e, ispr. i'dop. Moskva, Gos. nauchno-tekhn.ixd-vo mashinostroit. lit-ry, Vol.3, 1955. 563 p. (Mechanical engineering) (MLRA 8:12)

the street of th

VOL'MIR, Arnol'd Sergeyevich; SNITKO, I.K., redaktor; MURASHOVA, N.Ya., tokhnicheskiy redaktor

[Blectric buckling plates and shells] Gibkie plastiki i obelochki.

Moskva, Gos. izd-vo tekhniko-teoret. lit-ry, 1956. 419 p.(MIRA 9:11)

(Elastic plates and shells) (Buckling (Mechanics))

VOL'MIR, A.S., red.; NOVITSKIY, V.V. [translator]; SLABNOV, A.S. [translator]; GERMOGENOV, A.V., red.; IOVLEVA, N.A., tekhn, red.

[Theory of bending of circular plates] [Translated from the Chinese]
Teoriia gibkikh kruglykh plastinok. Moskva, Izd-vo inostr. lit-ry,
1957. 207 p.

(Blastic plates and shells)

THE PROPERTY OF THE PROPERTY O

AUTHOR TITLE

VOLIMIR, A.S.,

On the Influence of Initial Imperfections on the Stability of Cylincrical shells under External Pressure.

(O vliyanii nachal'nykh nepravil'nostey na ustoychivost'tsilindricheskikh obolochek pri vneshnem davlenii - Russian)

PERIODICAL

Doklady Akademii Nauk SSSR, 1957, Vol 113, Nr 2, pp 291-293, (U.S.S.R.) Received 6/1957

ABSTRACT

Reviewed 7/1957 A closed circular-cylindrical shell fortified on the front sides like a hinge is to be subjected to an evenly distributed external pressure. In the case of a deformation of the shell the cross-sections of the front sides are to remain circular, but the points of these cross-sections are to be able to suffer certain radical displacements. For investigating the stability of the shell the author applies on the whole the method of RITZ, and he approximates the function of deflection by means of the expression $\omega = f(\sin \alpha x \sin \beta y + \psi \sin^2 \alpha x + \psi)$. Here f denotes the maximum deflection, L - the longitude of the shell, R - its radius, n - the number of waves on its periphery. Moreover it is valid $\alpha=\pi/L$ and $\beta=\pi/R$. The shape of the central surface of the shell may differ a little from a circle before the beginning of the stress and the total deflection $\omega_{\mathbf{t}}$ may be composed of initial deflections ω_a and additional deflections. ω_{t} , $\omega_{g} + \omega = (f_{a}+f)(\sin \alpha x \sin \beta y + \psi \sin^{2}\alpha x + \psi)$ is to be valid. With such an assumption the influence of the original irregularities is especially clearly distinguished. Only the initial maximum deflection can be regarded as given. When producing real shells stresses of that kind

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On the Influence of Initial Imperfections on the Stability of Cylindrical Shells under External Pressure. PA - 3013

can actually appear. The computation of this deformation is discussed step by step. The results of these computations are shown in a diagram for the case R/h = 112,5, L/R = 2,2. On the occasion of deformation of a shell a detonation ought to occur under certain circumstances. With the existence of original irregularities the upper critical stress decreases. The lower limit, however, remains almost constant. If the initial maximum deflection enlarges the thickness of the shell, the stress varies monotonously. This and other conclusions are confirmed by tests with shells from duraluminum. (With 1 illustration).

ASSOCIATION SUBMITTED

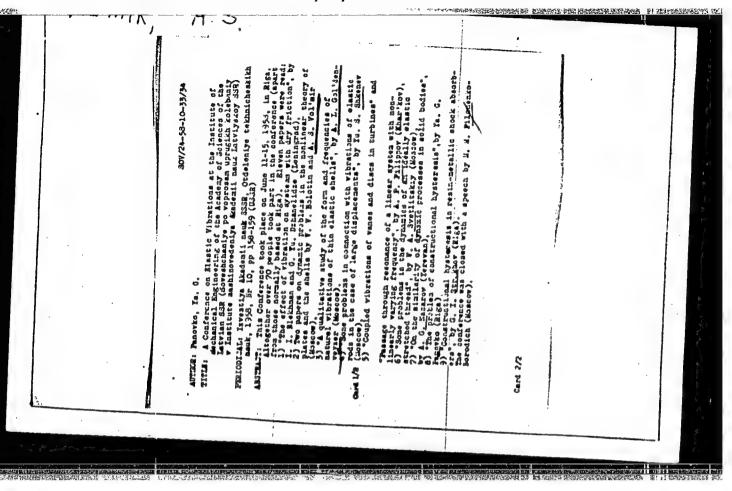
AVAILABLE

Card 2/2

Airforce-Engineer Academy "N.E. ZHUKOVSKIY" PRESENTED BY NEKRASOV, A.I., 15.10.1956

12.10.1956

Library of Congress



VOL'MIR, A.S.

24-58-3-4/38

AUTHOR: Bolotin, V. V. (Moscow)

Statistical Methods in the Non-Linear Theory of Elastic

Shells (Statisticheskiye metody v nelineynoy teorii uprugikh

opolochek)

PERIODICAL: Izvestiya Akademii Nauk SSSR. Otdeleniye Tekhnicheskikh Nauk, 1958, Nr 3, pp 33-41 (USSR)

In the non-linear theory of elastic shells two critical loads are distinguished, the lower, at which the bifurcation of the equilibrium shapes of the ideal shell occurs and the upper, where the initial type of elastic deflection first ceases to be unique. Experimentally measured buckling loads lie between the two according to the conditions and thoroughness of the test. A safe load may lie above the lower critical load, because an initial disturbance (deflection) sufficient to overcome the energy barrier separating one condition from the other, will not always be present. It has been pointed out that the lower critical load can be negative (Vol'mir, A.S., "Flexible Plates and Shells", Gostekhizdat, 1956). The "equal energy load" (Karman, Th. and Tsien, H.S., "The Buckling of Thin Cylindrical Shells under Axial Compression", J.Aeronaut.Sci., Vol.8, Nr 8, 1941) ignores the

initial deflection. On the other hand, the actual value of

24-58-3-4/38

Statistical Methods in the Non-Linear Theory of Elastic Shells.

the initial deflections is required in the Donnel method (Donnel L.H. and Wan C.C., "Effect of Imperfections on Buckling of Thin Cylinders", J.Appl.Mech. Nr 3,1950). The present paper introduces the statistical method to help in the prediction of the safe load and in the evaluation of buckling tests. In this approach, the initial deformation enters as one factor of a group embracing a finite number of parameters by which the state of the shell under load is defined. Most of the parameters are postulated to be random quantities. The statistical distribution law of these random quantities must be assumed but can sometimes be obtained from a sufficient number of tests. Statistical analysis is used to predict the mathematical expectation of the buckling of the shell under a given load. The practical importance of the statistical approach lies in the fact that the probability of buckling for a given multiple of the lower critical load varies predictably with the conditions of the problem. Moreover, the rate of increase of probability with the increase of the multiplying factor also depends on the nature of the shell and its fixing

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Statistical Methods in the Non-Linear Theory of Elastic Shells.

in a manner derivable by analysis. Furthermore, the analysis shows the degree of sensitivity of the probability of buckling in relation to the scatter in the initial disturbance (e.g., deformation). Thus a useful factor can be added to the pessimistic safe load, provided the initial deflections and their scatter are controllable. There are 7 illustrations, including 4 graphs, and 5 Soviet and 3 English references.

ASSOCIATION: Moskovskiy energeticheskiy institut (Moscow Power Institute)

SUBMITTED: October 14, 1957.

Card 3/3

1. Elastic shells -- Theory

14(10)

AUTHOR:

Vol'mir, A. S.

SOV/20-123-5-10/50

TITLE:

On the Stability of Cylindrical Shells Under Dynamic Loading (Ob ustoychivosti tsilindrichoskikh obolochek pri dinami-

cheskom nagruzhenii)

PERIODICAL:

Doklady Akademii nauk SSSR, 1958, Vol 123, Nr 5, pp 806-808

(USSR)

ABSTRACT:

An oblique circular cylindrical panel which has a certain initial sag is assumed to be quickly exposed to compressing stresses along the generatrix. The author investigates the time dependence of the deformation of the panel. The following system of differential equations is used for the descrip-

tion of great sags of a thin shell:

 $\frac{D}{h} \nabla^2 \nabla^2 \left(w_{\text{total}} - w_{\text{in}} \right) = w_{\text{total},xx} \Phi_{,yy} + w_{\text{total},yy} \Phi_{,xx} - \Phi_{,xx} + \Phi_{,xx} \Phi_{,xx} + \Phi_{,xx} \Phi_{,xx} \Phi_{,xx} + \Phi_{,xx} \Phi$

- $2w_{\text{total,xy}} \Phi_{,xy} + \frac{1}{R} \Phi_{,xx} - \frac{\gamma h}{g} w_{\text{total,tt}}$

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SOV/20-123-5-10/50 On the Stability of Cylindrical Shells Under Dynamic Loading

 $\frac{1}{E} \nabla^2 \nabla^2 \Phi = (w_{\text{total},xy})^2 - w_{\text{total},xx} w_{\text{total},yy} - (w_{\text{in},xy})^2 +$

+ Win,xx Win,yy $-\frac{1}{R}$ W,xx wtotal (x,y,t) denotes the total sag; Win(x,y) - the initial sag; Φ - a function of the stresses in the central surface of the shell; R - the radius of curvature of the central surface; h - the thickness of the shell; D - the cylindrical rigidity; γ - the specific weight of the substance; x,y - the coordinates read along the generatrix and along the arc; ∇ - the Laplace (Laplas) operator; and the indices after the comma - the differentiation with respect to the corresponding variable. The edges of the panel are assumed to be hinge-like open (sharnirno opertyy). The curved surface is approximately described by the expression Wtotal = ftotal sin($\pi x/a$) sin($\pi y/b$), where a and b denote the length and the breadth of the panel. A similar expression is assumed for the initial sag. The author investigates the case that the curved edges of the panel approach each to another with a given velocity c. It

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On the Stability of Cylindrical Shells Under Dynamic Loading

is assumed to be c
7 where 7 in the velocity of souri propagation in the shell substance. Formulae are deduced for the
mutual approximation of the edges and for the sag of a square
panel (a = b). The equation for the square panel was integrated
according to numerical methods by a computer of the type
MPT-9. 2 diagrams give the results of these calculations for
a plane plate and for a cylindrical panel. Similar results were
found by V. L. Agamirov and by the author for the case that
a closed circular cylindrical shell is exposed to an axial
compression or to a hydraulic pressure. There are 2 figures
and 3 Soviet references.

ASSOCIATION: Voyenno-vozdushnaya akademiya im. N. Ye. Zhukovskogo

(Air Force Academy imeni N. Ye. Zhukovskiy)

PRESENTED: July 4, 1958, by Yu. N. Rabotnov, Academician

SUBMITTED: June 26, 1958

Card 3/3

SEGAL', Aleksandr Iosifovich, prof., doktor tekhn, nauk; VOL'MIR, A.S., retsenzent; VITASHKINA, S.A., red.izd-va; IERMAKOVA, T.T., tekkn.red.

[Strength and stability of span coverings] Prochnost' i ustoichivost' sudovykh perekrytii. Izd.2., perer. i dop. Moskva, Izd.vo "Rechnoi transport," 1959. 515 p.

(Hulls (Haval architecture))

SOV/179-59-2-14/40

AUTHORS: Birkgan, A. Yu., Vol'mir, A. S. (Moscow)

Investigation of Large Deflections in Rectangular Plates by Means of a Digital Electronic Computer (Issledovaniye bol'-TITIE: shikh progibov pryamougol'noy plastinki pri pomoshchi tsifrovykh elektronnykh mashin)

PERIODICAL: Izvestiya Akademii nauk SSSR OTN, Mekhanika i mashino-stroyeniye, 1959, Nr 2, pp 100-106 (USSR)

There is little information available relating to the large deflections of plates, owing to the difficulty of ABSTRACT: integrating the relevant Karman system of non-linear differential equations. In the present paper, a digital electronic computer is applied to calculating the large deflection of a rectangular plate under the influence of a distributed lateral load. The basic equations and the boundary conditions are expressed as finite differences, and the solution obtained by successive approximations. The influence of the size of the mesh on the calculated values is investi-Tables and graphs are given containing values of the

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SOV/179-59-2-14/40

Investigation of Large Deflections in Rectangular Plates by Means of a Digital Electronic Computer

deflections of the stresses in the middle surface and of the bending stresses at certain characteristic points on the plate. The values agree with the results of investigations by other methods. There are 5 figures, 3 tables and 7 references, of which 5 are Soviet, 1 German and 1 English.

SUBMITTED: December 19, 1958.

Card 2/2

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sov/179-59-3-12/45
AUTHORS: Agamirov, V. L. and Vol'mir, A. S. (Moscow)
         Behaviour of Cylindrical Shells Under the Effect of a
         Dynamic Load Consisting of Overall Pressure or Axial
         Compression (Povedeniye tsilindricheskikh obolochek
TITLE:
         pri dinamicheskom nagruzhenii vsestoronnego davleniya
         ili osevogo szhatiya)
PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh
         nauk, Mekhanika i mashinostroyeniye, 1959, Nr 3,
ABSTRACT: It is assumed that the pressure rapidly increases. The
         pp 78-83 (USSR)
          equation of motion of elements of a shell is expressed
          as Eq (1.1) and the equation of deformation as Eq (1.2),
          where t - time,
          x and y - coordinates,
          w_{\underline{t}}(x,y,t) - full deflection (Eq 1.4),
          w_0(x,y) - initial deflection (Eq 1.3),
                   - function of the tension,
  Card 1/4 R and h - radius of the middle surface and the shell's
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sov/179-59-3-12/45

Behaviour of Cylindrical Shells Under the Effect of a Dynamic Load Consisting of Overall Pressure or Axial Compression

γ - specific weight of the material, q(t) - rate of an external pressure and $abla^2$ - two-dimensional Laplace operator. If Eqs (1.3) and (1.4) are substituted into Eq (1.2), then its integral can be represented as Eq (2.1) (Ref 10), the last two terms of which correspond to the tensions in the middle surface. The deformation of this surface can be The condition of calculated from Eq (2.3) or Eq (2.5). compactness in respect to the variable v has the form, Eq (2.6) which when substituted into Eq (2.5) will give the parameter φ (Eq 2.7) determined by the expressions These can be found from the Bubnov-Galerkin The relationship of the m and f1. parameters of deflection and the time can be derived from Eqs (4.1) and (4.2), which when substituted into Eq (3.4) will define the expressions (4.3) and (4.4), where V - velocity of elastic waves in the shell, Card $2/4 \zeta_1$ - the indicator of deflection (Eq 4.5).

sov/179-59-3-12/45

Behaviour of Cylindrical Shells Under the Effect of a Dynamic Load Consisting of Overall Pressure or Axial Compression

Figs 1 and 2 illustrate the function ζ₁ (t^o). The first group of curves in Fig 1 corresponds to the solution for c → 0 (Eq 4.3). The shape of the curve depends on the number of waves n generated by buckling of the shell (e.g. point A, n = 6). The second group of curves represents the value of n for the dynamic load with rate of pressure increase c = 2 x 10³ atm/sec. The value of t^o (Eq 4.2) determines the ratio of the variable pressure q to its critical value q for a given n.

Fig 2 illustrates two other groups of curves corresponding to c = 10⁴ and c = 2 x 10⁴ atm/sec. Similar results were obtained for the case where the dynamic load was in the form of the axial compression, i.e. q = 0 in Eq (1.1). The values of the initial and total deflections in this case can be calculated from Eq (6.1) and the various parameters found from Eq (6.2). An expression of the Eq (4.3) type in this case will have the form of Eqs (6.3) and (6.4). The parameter ψ can be determined from Eq (3.2).

sov/179-59-3-12/45

Behaviour of Cylindrical Shalls Under the Effect of a Dynamic Load Consisting of Overall Pressure or Axial Compression

Same as that in the first case.

There are 2 figures and 11 references, 6 of which are Soviet, 4 English and 1 German.

SUBMITTED: December 19, 1958

Card 4/4

14 (10) AUTHORS: Vol'mir, A. S., Mineyev, V. Ye.

507/20-125-5-13/61

TITLE:

The Experimental Investigation of the Process of the Buckling of a Shell Under a Dynamic Load (Eksperimental'neye issledovaniye protsessa vypuchivaniya obolochki pri dinamicheskom

nagruzhenii)

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 125, Nr 5, pp 1002 - 1003

(USSR)

ABSTRACT:

M. A. Lavrent'yev and A. Yu. Ishlinskiy (Ref 1) described an experiment in which a cylindrical tube was suddenly compressed by the application of water pressure. In those parts of the tube which were located in closer proximity of the source of disturbance, greater V stability losses were observed. The present paper describes the results obtained by experiments in which such an effect was quantitatively evaluated. The experimental arrangement consisted of 2 reservoirs which were arranged so that one contained the other, and were filled with oil. The sample, which had the shape of a round cylindrical shell, is located in the inner reservoir, and the upper frontal surface remains free. In the outer reservoir increased pressure (5 to 50 at) is generated. The sudden opening of the valve

Card 1/3

The Experimental Investigation of the Process of the SOV/20-125-5-13/61. Buckling of a Shell Under a Dynamic Load

in the inner reservoir causes a hydraulic shock which is conveyed to the sample. The time dependence of pressure in some points of the reservoir is measured by means of special primary elements, and the signals originating from it are recorded on the band of a loop oscillograph. The primary elements of chmic resistance fastened to the outer and inner surfaces of the sample make it possible to measure the elongations at the corresponding points. Also the deflections of these primary elements were transmitted to the oscillograph. In these experiments the pressure difference between the cuter and the inner reservoir and also the time, during which the valve remains open was varied, so that it was possible to attain various rates at which pressure increased (within the limits of from 2000 to 6500 at/sec). The oscillogram for testing one of these samples is shown by a figure. In the first period of dynamic load the deformations have the same sign (acceleration). Then the deformation of the inner surface quickly changes its sign, and this corresponds to the instant of time at which the shell becomes buckled. For some samples the critical load was determined as a function of the rate at which pressure in-

Card 2/3

The Experimental Investigation of the Process of the S07/20-125-5-13/61. Buckling of a Shell Under a Dynamic Load

creased. Besides, a table shows the coefficient of dynamic load. With increasing loading speed the form of wave-formation changes, and this manifests itself also by the increase of the number of waves on the periphery. Besides, the bearing capacity of the shell at the stage of being under load increases considerably. These data correspond to the results obtained by solving the nonlinear problem of the stability of the shells under dynamic load. V. S. Smirnov assisted in cerrying out the experiments. There are 2 figures, 1 table, and 3 Soviet references.

ASSOCIATION:

Voyenno-vozdushnaya inzhenernaya akademiya in. N. Ye. Zhukovskego

(Academy for Air-force Engineers imeni N. Ye. Zhukovskiy)

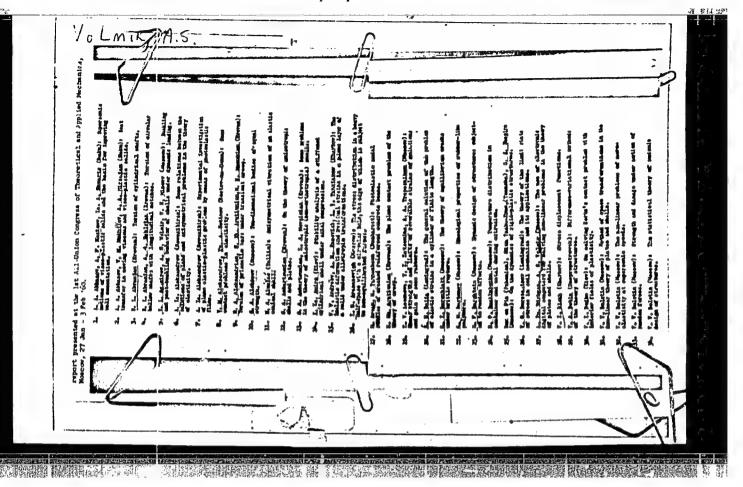
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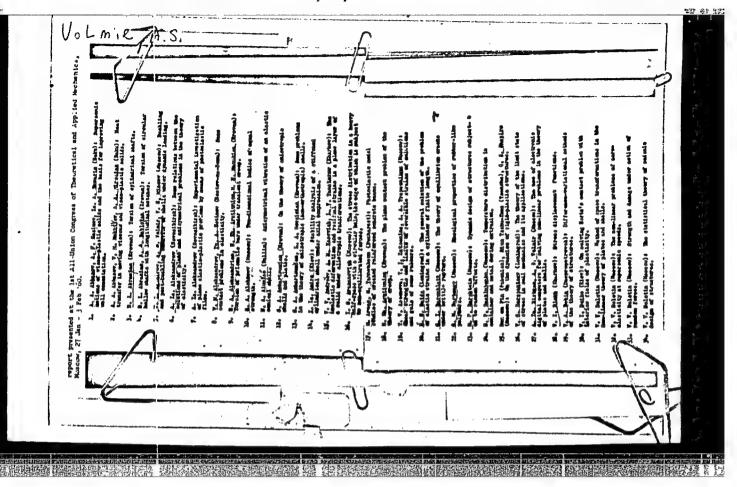
December 23, 1958, by Yu. N. Rabotnov, Academician

SUBMITTED:

December 23, 1958

Card 3/3





MUSHTARI, Kh.M., red.; ALUMYAE, N.A., red.; BOLOTIN, V.V., red.;

VOL'MIR, A.S., red.; GANIYEV, N.S., red.; GOL'DENVEYZER,

A.L., red.; ISANBAYEVA, F.S., red.; KIL'CHEVSKIY, H.A.,

red.; KORNISHIN, M.S., red.; LUR'YE, M.I., red.; SAVIN,

G.N., red.; SACHENKOV, A.V., red.; SVIRSKIY, I.V., red.;

SURKIN, R.G., red.; FILIPPOV, A.P., red.; ALEKSAGIN, V.I.,

red.; SEMENOV, Yu.P., tekhn. red.

[Proceedings of the Conference on the Theory of Plates and Shells] Trudy Konferentsii po teorii plastin i obolochek, Kassani, 1960. Kazani, Akad. nauk SSSR, Kazanskii filial, 1960. (MIRA 15:7)

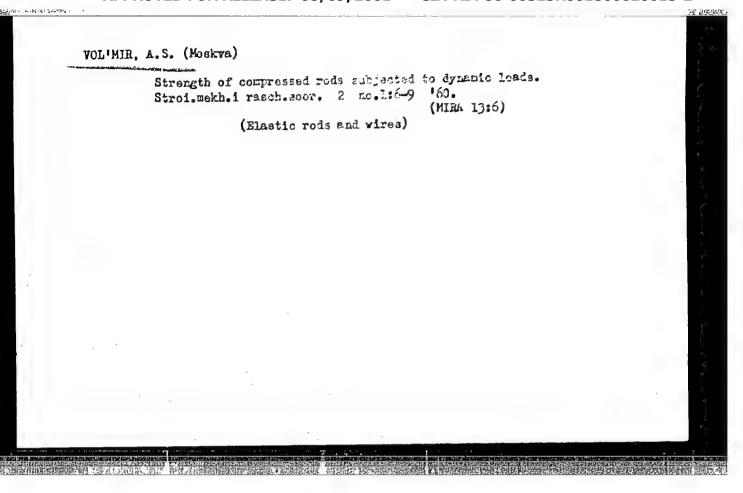
- 1. Konferentsiya po teorii plastin i obolochek, Kazan', 1960. 2. Moskovskiy energeticheskiy institut (for Bolotin). 3. Kazanskiy khimiko tekhnologicheskiy institut (for Ganiyev). 4. Institut mekhaniki Akademii nauk USSR (for Kilichevskiy).
- 5. Kazanskiy gosudarstvennyy universitet (for Sachenkov).
- 6. Kazanskiy filial Akademii nauk SSSR (for Svirskiy). (Elastic plates and shells)

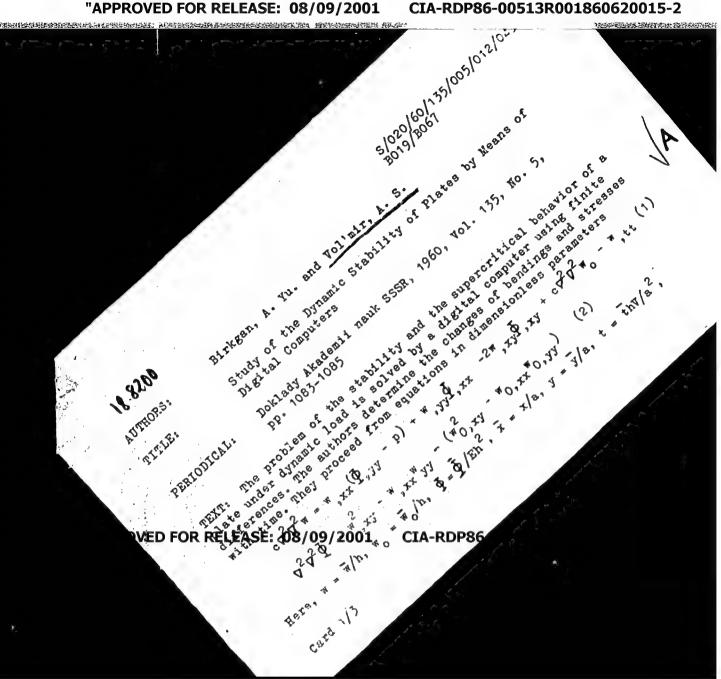
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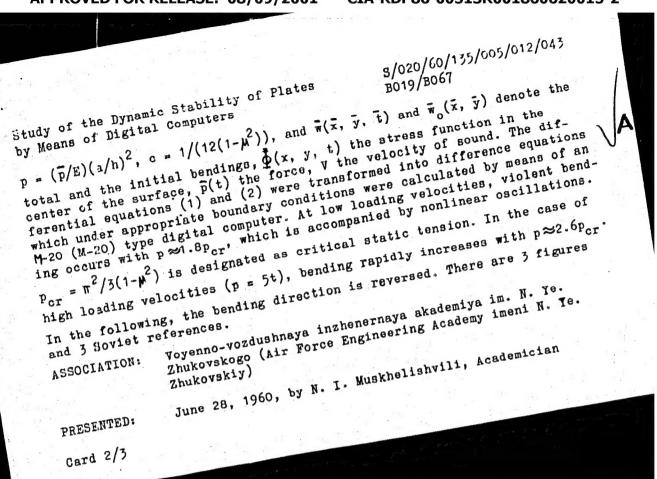
VOLMIR, A. S. (Moscow)

"Stability and Postbuckling Behaviour of Shells under Dynamic Loading."

report submitted for the Xth International Congress of Applied Mechanics, Stresa, Italy, 31 Aug - 7 Sep 60.







"APPROVED FOR RELEASE: 08/09/2001 CIA-RDP86-00513R001860620015-2

Study of the Dynamic Stability of Plates by Means of Digital Computers

SUBMITTED: June 10, 1960.

Card 3/2

s/779/61/000/006/001/003 1071/1242

Vol'mir, A.S., Prof., Dr. of Technical Sciences (Moscow) AUTHOR:

The stability of plates under plastic deformation TITLE:

Raschet prostranstvennych konstruktsiy; sbornik SOURCE:

statey, no.6, Moscow, 1961, 149-188

Stability means the absence of infinitely close stable positions. The problem is studied with the help of the theory of elastic-plastic deformations (non-linear clasticity) and the theory of flow. The principal results in the first theory were obtained by Ilyushin and in the second by Prager, by Pearson and by Katchanov. The chapter headings are: 1. Applications of plasticity theory to problems of stability plates. 2. Theory of deformations. Fundamental relations. 3. Basic differential relation in the case of incompress-

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The stability of plates under ...

ible material. A. Application of variation methods. 5. Stability of a freely supported plate compressed in one direction. 6. Establishment of the basic equation without consideration of the unloading effect. 7. Uniaxial compression of a freely supported plate. 8. Other boundary conditions. 9. Stability of a plate under deformation. 10. Generalization of the deformation theory for the case of compressible material. 11. Fundamental relations of flow theory. 12. Solution of particular problems. 13. Influence of compressibility in flow theory. 14. Computational data for duraluminum and steel. 15. Data for practical computations. Experiments show that, as with bars, the critical values computed by the flow theory are higher while those computed by the theory of elasto-plastic deformations are lower than the experimental. Except for plates with initial irregularities, the latter theory is preferred. There are 33 references.

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